

## Level 3 Spice from Depletion-Region Approximation Referred to Source

Taylor Series Expansion Parameter

$$\alpha_s = 1 + \frac{\gamma}{2\sqrt{\psi_{sS}}} \quad 1$$

$$V_T = V_{FB} + \psi_{sS} + \gamma\sqrt{\psi_{sS}} \quad 2$$

$$V_P = \frac{V_G - V_T}{\alpha_s} \quad 3$$

$$V_{IS} = \alpha_s V_{Ps} \quad 4$$

$$V_{ID} = \alpha_s [V_P - (\psi_{sD} - \psi_{sS})] \quad 5$$

With depletion-region approximation, general.

$$i_{Ddrift} = \frac{1}{2\alpha_s} (V_{IS}^2 - V_{ID}^2) \quad 6$$

Source-reference case.

$$i_{Ddrift} = \frac{\alpha_s}{2} [V_P^2 - (V_P - (\psi_{sD} - \psi_{sS}))^2] \quad 7$$

$$i_{Ddrift} = \alpha_s \left[ V_P (\psi_{sD} - \psi_{sS}) - \frac{(\psi_{sD} - \psi_{sS})^2}{2} \right] \quad 8$$

Strong Inversion – Level 3

$$V_{GS} = V_G - V_S \quad 9$$

$$\psi_{sD} - \psi_{sS} = V_D - V_S = V_{DS} \quad 10$$

Threshold Voltage Referred to Source

$$V_P = \frac{V_G - (V_{FB} + PHI + V_S + \gamma\sqrt{PHI + V_S})}{\alpha_s} = \frac{V_{GS} - (V_{FB} + PHI + \gamma\sqrt{PHI + V_S})}{\alpha_s} \quad 11$$

$$V_{TO} = V_{FB} + PHI + \gamma\sqrt{PHI} \quad 12$$

$$V_T = V_{FB} + PHI + \gamma\sqrt{PHI + V_S} = V_{TO} + \gamma(\sqrt{PHI + V_S} - \sqrt{PHI}) \quad 13$$

$$\alpha_s = 1 + \frac{\gamma}{2\sqrt{PHI + V_S}} \quad 14$$

$$i_D = \alpha_s \left( V_P V_{DS} - \frac{V_{DS}^2}{2} \right) \quad 15$$

$$i_D = (V_G - V_{Ts}) V_{DS} - \alpha_s \frac{V_{DS}^2}{2} \quad 16$$

At Saturation

$$i_D = \frac{\alpha_s}{2} V_P^2 \quad 17$$

$$I_{Dsat} = UO \cdot COX \frac{W}{L_{eff}} i_D \quad 18$$

Channel-Length Modulation

$$z = \sqrt{\frac{2\epsilon_s}{qN_{sub}}} \quad 19$$

$$V_{DS} = V_{DS} > V_{dsat} \quad V_{DS} : V_{dsat} \quad (I_p = 0 \text{ in Pre-Sat, } L = L_{eff})$$

$$I_p = z\sqrt{KAPPA(V_{DS} - V_{Dsat})} \quad 20$$

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$$L = L_{\text{eff}} - l_p \quad 21$$

$$I_D = UO \cdot COX \frac{W}{L} i_D \quad 22$$

VMAX  $\neq$  0, Include Mobility Reduction Effects in General

$$UCRIT = \frac{VMAX}{UO} \quad 23$$

$$V_C = UCRIT \cdot L_{\text{eff}} \quad 24$$

Mobility Reduction due to Vertical Electric Field

$$U_b = \frac{UO}{1 + \text{THETA}(V_{GS} - V_T)} \quad 25$$

$$V_b = [1 + (V_{GS} - V_T)\text{THETA}]V_C \quad 26$$

Reduced Saturation Voltage

$$V_{\text{dsat}} = V_{D\text{sat}} + V_b - \sqrt{V_{D\text{sat}}^2 + V_b^2} \quad 27$$

Channel-Length Modulation with VMAX  $\neq$  0

$$V_{\text{ds}} = V_{DS} > V_{\text{dsat}} \quad ?V_{\text{dsat}} : V_{DS} \quad 28$$

$$E_P = \frac{KAPPA}{L_{\text{eff}}} \left[ \frac{i_{Dx}}{(V_{D\text{sat}} - V_{\text{ds}}) - \frac{i_{Dx}}{V_b + V_{\text{ds}}}} \right] \quad 29$$

$$i_{Dx} = \left[ V_{D\text{sat}} V_{\text{ds}} - \frac{1}{2} V_{\text{ds}}^2 \right] \quad 30$$

$$l_c = \frac{z^2 E_P}{2} \quad 31$$

$$V_{DS} = V_{DS} > V_{\text{dsat}} \quad ?V_{DS} : V_{\text{dsat}} \quad 32$$

$$I_p = z\sqrt{KAPPA(V_{DS} - V_{Dsat})} \quad \text{Eq. 20}$$

$$L_p = \sqrt{I_c^2 + I_p^2} - I_c^2 \quad 33$$

$$L = L_{eff} - L_p \quad 34$$

$$I_D = U_{eff} \cdot COX \frac{W}{L} i_D \quad 35$$

$$V_{ds} = V_{DS} > V_{dsat} \quad ? V_{dsat} : V_{DS} \quad 36$$

$$U_{eff} = \frac{U_b}{1 + \frac{V_{ds}}{V_b}} \quad 37$$

$$COX = \frac{\epsilon_i}{t_{ox}} \quad 38$$

$V_{dsat0}$  Based on Slope of ID = Zero.  $V_{dsat0} > V_{dsat}$

$$V_{dsat0} = \left[ \sqrt{\frac{2V_{Dsat}}{V_b} + 1} - 1 \right] V_b \quad 39$$

Alternate Form -  $V_{dsat} \rightarrow V_{dsat0}$  for large  $V_b$  or  $KAPPA \rightarrow \infty$  for finite slope.

$$V_{dsat0} = V_{Dsat0} + V_b \left( 1 + \frac{V_{dsat0}}{V_b} \right) - \sqrt{V_{Dsat}^2 + \left[ V_b \left( 1 + \frac{V_{dsat0}}{V_b} \right) \right]^2} \quad 40$$

Drain and Source Series Resistance  $R_S$  and  $R_D$

$V_{GS}$ ,  $V_{DS}$ ,  $V_S$  measured, externally applied.

$$V_{GS}' = V_{GS} - I_D R_S \quad 41$$

$$V_S' = V_S + I_D R_S \quad 42$$

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$$V_{DS}' = V_{DS} - I_D R_S - I_D R_D \quad 43$$

Static Feedback -  $V_{DS}' = V_{DS} - I_D R_S - I_D R_D$

$$V_{DS}' = V_{DS} - I_D R_S - I_D R_D \quad 44$$

DIBL - ETA

$$V_T = V_T - \text{ETA} \cdot \sigma \cdot V_{DS} \quad 45$$

$$\sigma = \frac{8.15 \cdot 10^{-22}}{C_{\text{ox}} L_{\text{eff}}^3} \quad 46$$